

Subsurface Investigation Report

Proposed Four Story Building

Located At

**19305 Gulf Blvd.
Indian Shores, Pinellas County, Florida**

January 2010

Prepared for

**Town of Indian Shores
19305 Gulf Blvd.
Indian Shores, FL 33785**

GULF COAST TESTING LABORATORY INC.
5745 Park Boulevard North
PINELLAS PARK, FL 33781
CONSTRUCTION MATERIALS ENGINEERING COUNCIL CERTIFIED
PHONE: (727) 544:4080 FAX: (727) 544:7532

GULF COAST TESTING LABORATORY INC.

5745 PARK BOULEVARD

PINELLAS PARK, FL 33781

CONSTRUCTION MATERIALS ENGINEERING COUNCIL CERTIFIED

CERTIFICATE of AUTHORIZATION # 00002370

PHONE: (727) 544-4080 FAX: (727) 544-7532

January 19, 2010
Lab #16408

Town of Indian Shores
19305 Gulf Blvd.
Indian Shores, FL 33785

Attention: Mr. Lawrence Nayman

RE: Subsurface Investigation
Proposed Four Story Building
19305 Gulf Blvd.
Indian Shores, Pinellas County, Florida 33785

Gentlemen:

Gulf Coast Testing Laboratory, Inc. has completed the subsurface investigation in the above referenced site as authorized in accordance with our proposal letter dated November 13, 2009.

Due to the existing one story structure, the three Standard Penetration Test borings had to be located at the north side, the west side and south sides of the proposed building at the approximate locations as indicated on the pre-marked building drawing as supplied to our office by Mr. Nayman. The approximate locations of these three borings are shown on the attached sketch.

The test borings B-1 and B-2 were taken to depths of 40 feet below the existing round surface. The test boring B-3 was taken to a depth of 35 feet below the existing ground surface.

This report presents the soil test data along with our evaluation for the pile foundation support for the proposed four story building.

SOIL EXPLORATION METHOD

The three test borings performed in this site were made in accordance with ASTM D-1586 "Penetration Test and Split Barrel Sampling of Soils". Rotary drilling was used to advance the best borings. No casings were required in these borings.

The Standard Penetration Resistance (N) is the number of blows of a 140 pound hammer falling 30 inches to drive a 2 inch outer diameter/1.4 inch inner diameter, split spoon sampler, one foot.

The sampler was initially seated 6 inches to penetrate any loose cuttings, whereupon the number of blows, required to produce the next foot of penetration was recorded. A representative of this firm

classified the samples in the field as they were obtained and a representative portion of each sample type were then sealed and transferred to our facility for further verification.

The soil samples will be retained by the engineering facility for a period of 90 days from the date of this report, and then disposed of, unless otherwise notified.

SITE CONDITIONS AND SUBSOIL OBSERVATIONS

The property is located east of Gulf Blvd. and west of the Inter Coastal Waterway in the Town of Indian Shores, Pinellas County, Florida. The proposed building area is located behind the existing city buildings and there are existing one story structures in the proposed building area. As explained earlier, the three test borings were located in the accessible areas and the site surface at these boring locations was either paved area or landscaped area. Due to the possible underground utility lines in this area, a shallow hand auger boring was done at each boring location to a depth of 4 feet below the existing ground surface and then the Standard Penetration Test boring involving rotary drilling operations was done in these locations.

In general, all the three test borings encountered sands with variable amounts of shell fragments in the shallow depth range of $6\pm$ feet below the existing ground surface. The upper layer of mostly loose sands is underlain by loose layer of sand with silt and organic particles to approximately $12\pm$ feet depth below the existing ground surface.

A very loose stratum of sandy silt with shell fragments was found in all the three borings below 12± feet to approximately 18 feet depth. This very weak stratum is underlain by loose layers of silty sands with shells to approximately $22\pm$ feet depth.

The test boring B-1 encountered a stiff layer of sandy clay between $22\pm$ feet and $27\pm$ feet depth range, but the test borings B-2 and B-3 encountered loose and medium layer of clayey sand in this depth range.

Below $27\pm$ feet to the terminated depth of 40 feet, the test borings B-1 and B-2 indicated multiple erratic layers of clayey sand to very clayey sand and very sandy clay and the consistency or relative density varied from stiff to hard or very dense. The test boring B-3 also encountered similar erratic layers of clayey sand with phosphate particles below $27\pm$ feet to the terminated depth of 35 feet. In general, the stratum between 35 feet and 40 feet was mostly hard in these locations.

The ground water level was found at 3 feet 11 inches below the existing ground surface in this site. The tidal variations in the nearby waterway will influence the ground water depth in this site.

EVALUATION FOR THE FOUNDATION SUPPORT

We understand that the proposed building will be a four story masonry block/concrete structure consisting of three living levels above ground level parking. It was further indicated to us that all the suspended living level and the roof level would have concrete floors. We recommend that the proposed four story structure should be supported by a suitable pile supported grade beam pile cap system. We consider that the ground floor slab may be soil supported, (suitably well compacted to a minimum of 95% of the Modified Proctor Density) if design considerations are taken to permit separation of the floor slab from the building allowing for small differential settlement.

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We discussed the choice of using different types of piles for this project with the structural engineer. We also furnish the advantages and disadvantages of using pre-cast concrete piles over the augered cast-in-place piles in this project.

We present the evaluation for both types of piles in this report for consideration.

PRE-CAST CONCRETE PILES

We consider that typical 12 inch by 12 inch pre-cast concrete pile, driven to a depth range of 30 to 35 feet below the existing ground surface, should have a safe compressive capacity of 30 tons. A safe uplift capacity of 7 tons may be appropriate for design purposes.

It should be noted that between the depth range of 25 feet and 35 feet below the existing ground surface, intermittent layers of hard cemented clay and stiff layers of sandy clay and/or clay with silty clay lenses were found in all three of the boring locations. Such stratification of varying consistency appears to be common in this site at varying depth ranges; therefore, it is possible that resistance to driving these pre-cast concrete piles may be encountered at varying depth levels at different locations. It is therefore prudent to consider whether a driven pile is suited to this site such as this, where variable pile lengths are anticipated.

If a higher capacity piles are contemplated, we consider that a typical 14 inch by 14 inch pre-cast concrete pile driven to the same depth range of 30 to 35 feet below the existing ground surface, should have a safe compressive capacity of 35 tons. A safe uplift capacity of 8.5 tons may be appropriate for design purpose. A lateral capacity of not greater than 2 tons may be appropriate for these pre-cast concrete piles.

These piles should be driven with a suitable hammer compatible with the type of pile being driven and also taking into consideration the proximity to the nearby existing structures. An engineer's representative should verify the capacity of each pile by monitoring and recording the driving resistance during the pile driving operations. The capacity of the pile should be estimated using an appropriate pile driving formula in accordance with local building code regulations.

Prior to the start of production pile installation, a tentative pile driving resistance program (involving some test piles driven at the building area) may be computed using any of the widely used dynamic formulas, which also should be verified by at least one static load test. The static load test should be conducted on the test pile in accordance with ASTM D-1143, Standard Method. Unlike augered cast-in-place piles, pre-cast concrete piles are difficult to cut and splice, therefore the test pile program will enable a proper decision to be made regarding suitable lengths of the production piles.

AUGERED CAST-IN-PLACE PILES

We also consider that the proposed four story building can be supported by Augered Cast-in-Place piles, where there will be no impact of pile driving in the nearby area and no pile cut off process will be required. We consider that an Augered Cast-in-Place pile, 14 inches in diameter, installed to a depth range of $30\pm$ to $35\pm$ feet below the existing ground surface, should have a safe compressive capacity of 30 tons.

The test borings indicated a cohesive soil stratum of varying consistency and relative density of clayey sand between the 25 and 35 foot depth range; however the installed depth may vary outside this depth range.

The drilled and installed depth of these augered cast-in-place piles may vary in this site due to the underlying erratic soil layers. It should be noted that the upper very weak stratum of silty soils would require a considerable amount of grout, more than the theoretical volume.

Prior to the commencement of production pile installation, we recommend tentative test drilling and installation of a test pile in this area will be appropriate followed by a static load test conducted in accordance with ASTM D-1143.

It is further recommended that an engineer's representative monitor the installation of these augered cast-in-place piles and that pile log records be kept to verify the design capacity of each pile.

We consider that these piles develop their capacity by a combination of skin friction and end bearing. An experienced contractor should install these augered cast-in-place piles. Depending on the relative density of the underlying clayey sand soils or the consistency of the cemented clay at different locations, some variations in the installed depth of these piles should be anticipated.

IN CONCLUSION

The analysis and recommendation of this report are based on the data obtained from the three test borings conducted at the approximate locations as indicated on the enclosed sketch. Variations in stratification of soils and fluctuations in the ground water table should be anticipated. If, during construction, conditions other than those noted herein are encountered, we must be notified immediately to re-evaluate the recommendations of this report, and make changes and/or adjustments, if necessary.

We appreciate the opportunity of providing this service to you. Should you have any questions regarding this report, or if we may be of further assistance to you on this project or any other, please contact our office.

Respectfully submitted,

GULF COAST TESTING LABORATORY, INC.



R. Gunasekaran, P.E.
Fla. License No. 20402

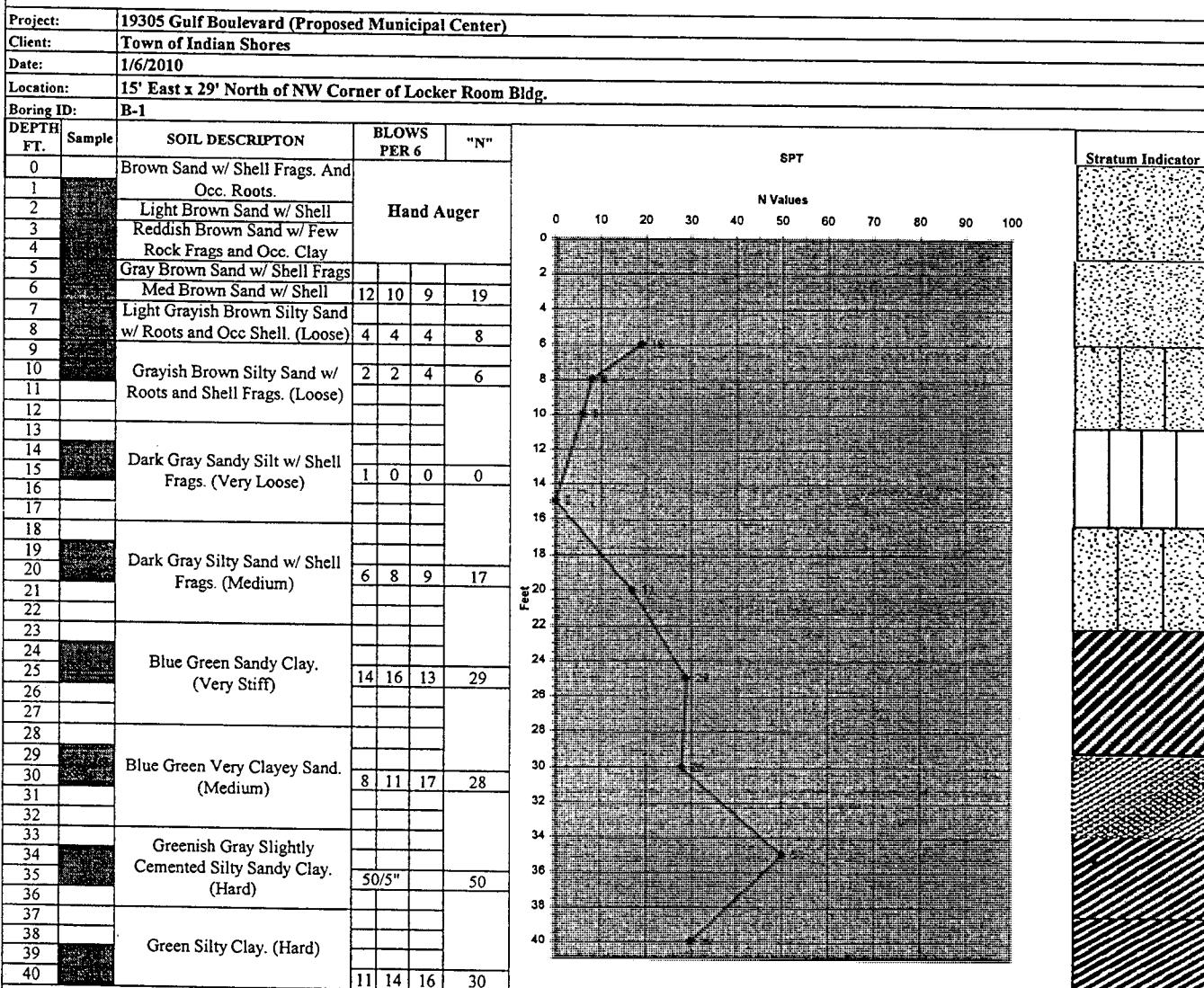
1/19/10

Gulf Coast Testing Laboratory, Inc.

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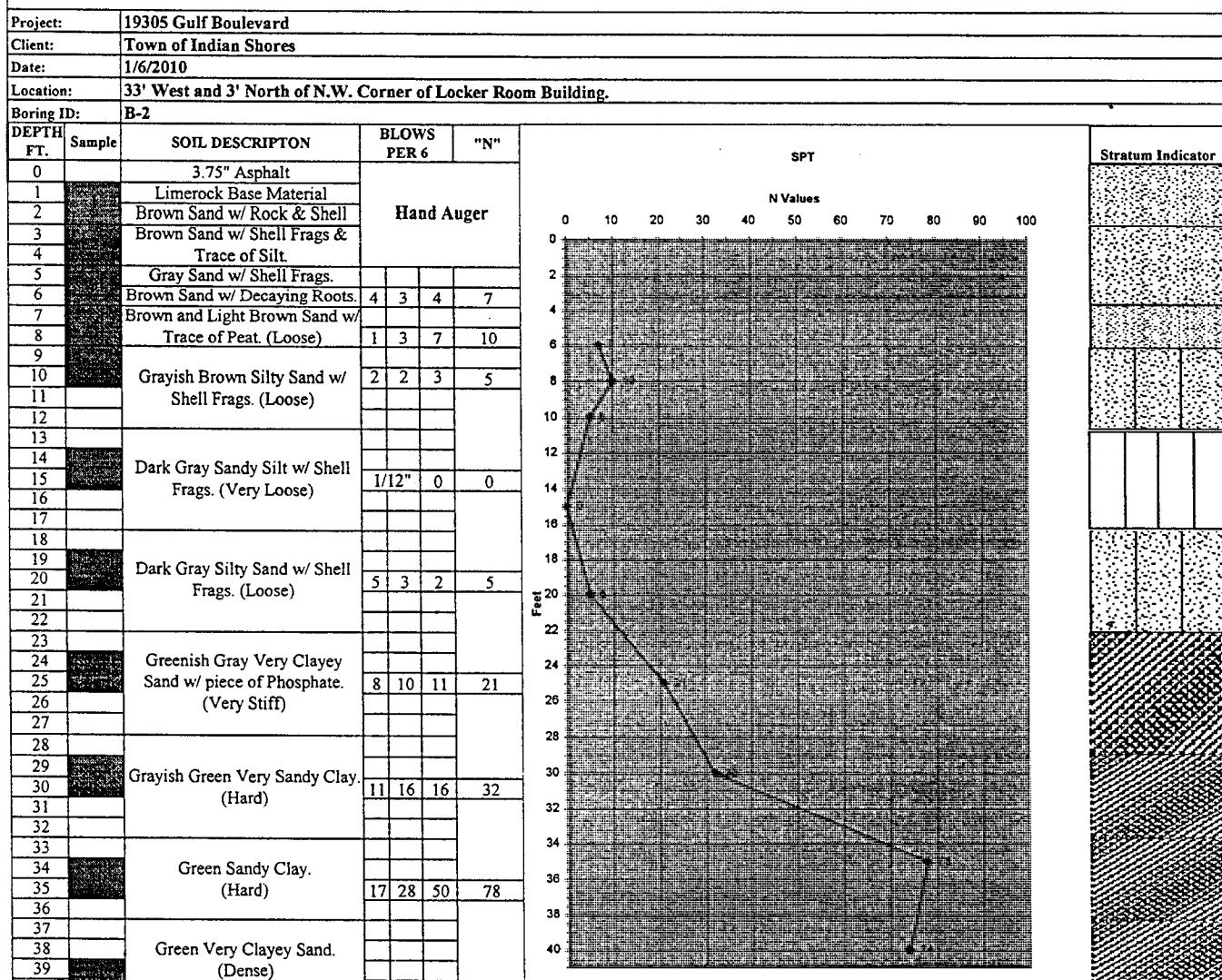


Boring Terminated @ 40'

| | | | | | | |
|---------------------|--------|--|-------------------------------|-------------|-------------|--|
| Remarks | | Material descriptions are based on visual observations and not laboratory test procedures. The materials between the sampling elevations may vary. Any recommendations, solutions, or other representations are based on the available information and subject to change if other materials are encountered during the installation of any foundation systems developed from this information. | | | | |
| Lab # | 16408 | | Method of Sampling: | ASTM D-1586 | | |
| Ground Water Depth: | HA 47" | Hammer Weight: | 140 pounds | Fall: | 30 - inches | |
| Length Of Casing: | N/A | Sampler: | 1.4" I.D. Split Spoon Sampler | | | |

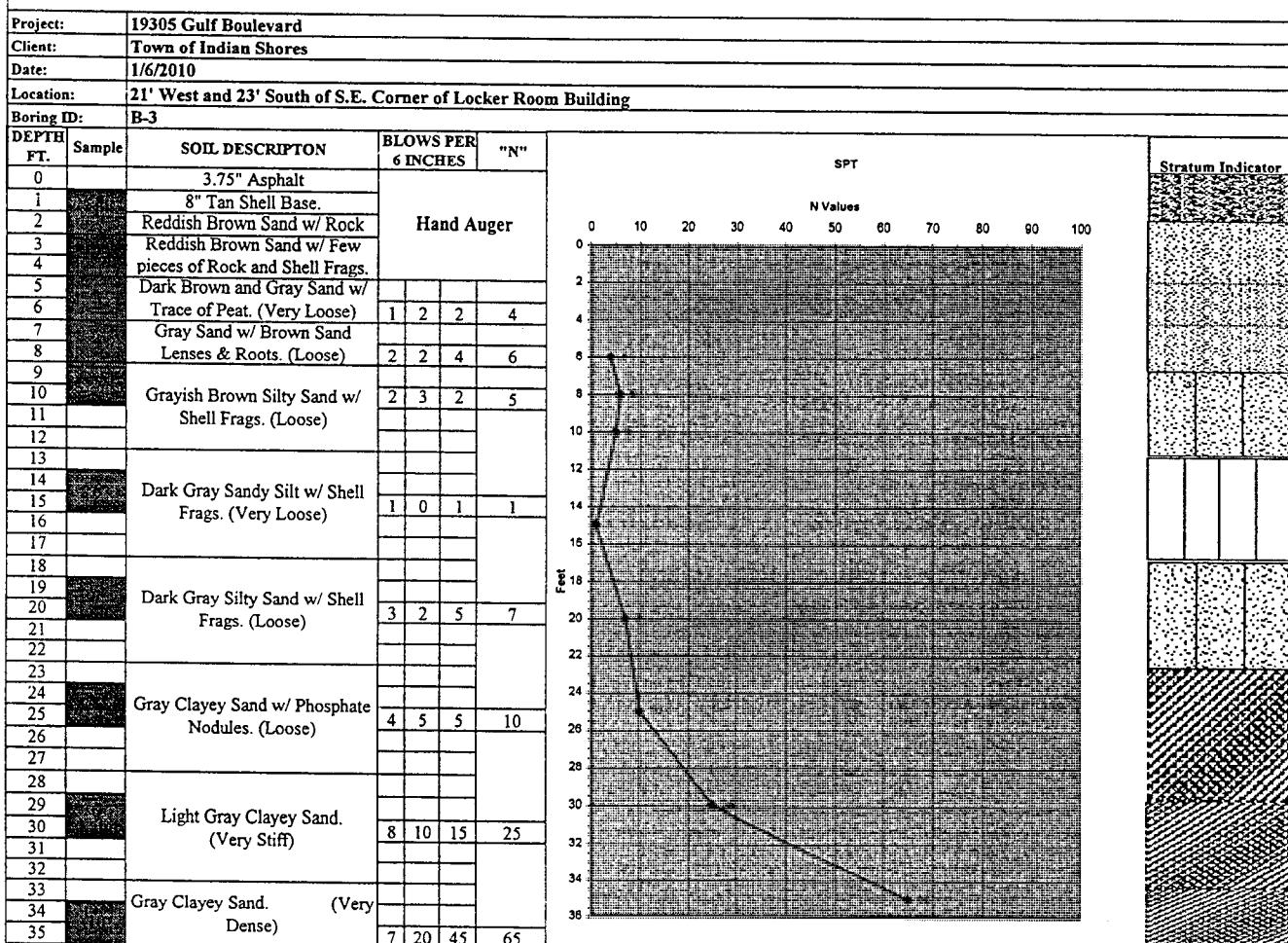
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Boring Terminated @ 35'

| | | | | | | | | | | | | | |
|---------------------|-------|--|-------------------------------|-------|-------------|--|--|--|--|--|--|--|--|
| Remarks | | Material descriptions are based on visual observations and not laboratory test procedures. The materials between the sampling elevations may vary. Any recommendations, solutions, or other representations are based on the available information and subject to change if other materials are encountered during the installation of any foundation systems developed from this information. | | | | | | | | | | | |
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CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES
ASTM Designation: D 2487 - 83
(Based on Unified Soil Classification System)

**SOIL
CLASSIFICATION**

| Criteria for Assigning Group Symbols and Group Names Using Laboratory Tests* | | | | Soil Classification | |
|--|--|---|---|---------------------|----------------------|
| | | | | Group Symbol | Group Name* |
| Coarse-Grained Soils (More than 50% retained on No. 200 sieve) | Gravels More than 50% coarse fraction retained on No. 4 sieve | Clean Gravels Less than 5% fines | $Cu \geq 4$ and $1 \leq Cc \leq 3$ | GW | Well graded gravel |
| | | | $Cu < 4$ and/or $1 > Cc > 3$ | GP | Poorly graded gravel |
| | | Gravels with Fines More than 12% fines | Fines classify as ML or MH | GM | Silty gravel *** |
| | | | Fines classify as CL or CH | GC | Clayey gravel *** |
| | Sands 50% or more of coarse fraction passes No. 4 sieve | Clean Sands Less than 5% fines | $Cu \geq 6$ and $1 \leq Cc \leq 3$ | SW | Well-graded sand |
| | | | $Cu < 6$ and/or $1 > Cc > 3$ | SP | Poorly graded sand |
| | | Sands with Fines More than 12% fines | Fines classify as ML or MH | SM | Silty sand *** |
| | | | Fines classify as CL or CH | SC | Clayey sand *** |
| Fine-Grained Soils (50% or more passes the No. 200 sieve) | Sils and Clays Liquid limit less than 50 | Inorganic | $PI > 7$ and plots on or above "A" line | CL | Lean clay *** |
| | | | $PI < 4$ or plots below "A" line | ML | Silt *** |
| | | Organic | $\frac{\text{Liquid limit - oven dried}}{\text{Liquid limit - not dried}} < 0.75$ | OL | Organic clay *** |
| | | | | | Organic silt *** |
| | Sils and Clays Liquid limit 50 or more | Inorganic | PI plots on or above "A" line | CH | Fat clay *** |
| | | | PI plots below "A" line | MH | Elastic silt *** |
| | | Organic | $\frac{\text{Liquid limit - oven dried}}{\text{Liquid limit - not dried}} < 0.75$ | OH | Organic clay *** |
| | | | | | Organic silt *** |
| Highly organic soils | Primarily organic matter, dark in color and organic odor | | | | PT Peat |

*Based on the material passing the 3-in. (75-mm) sieve.

**If field sample contained cobbles or boulders, or both, add "with cobbles or boulders, or both" to group name.

**Gravels with 5 to 12% fines require dual symbols:

GW-GM well-graded gravel with silt

GW-GC well-graded gravel with clay

GP-GM poorly graded gravel with silt

GP-GC poorly graded gravel with clay

**Sands with 5 to 12% fines require dual symbols:

SW-SM well-graded sand with silt

SW-SC well-graded sand with clay

SP-SM poorly graded sand with silt

SP-SC poorly graded sand with clay

**DESCRIPTIVE ADJECTIVES for
COARSE and FINE GRAINED SOILS***

| Descriptive Adjective | Percentage Requirements |
|-----------------------|-------------------------|
| trace | Under 5% |
| few | 5 - 15% |
| little | 15 - 30% |
| some | 30 - 50% |
| mostly | 50 - 100% |

*Modified from ASTM-D 2488-84

$$Cu = D_{30}/D_{10}, Cc = \frac{(D_{30})^2}{D_{10} \times D_{60}}$$

If soil contains $\geq 15\%$ sand, add "with sand" to group name.

If fines classify as CL-ML use dual symbol GC-GM or SC-SM.

If fines are organic, add "with organic fines" to group name.

If soil contains $\geq 15\%$ gravel, add "with gravel" to group name.

If Atterberg limits plot in hatched area, soil is a CL-ML silty clay.

If soil contains 15 to 25% plus No. 200, add "with sand" or "with gravel," whichever is predominant.

If soil contains $\geq 30\%$ plus No. 200, predominantly sand, add "sandy" to group name.

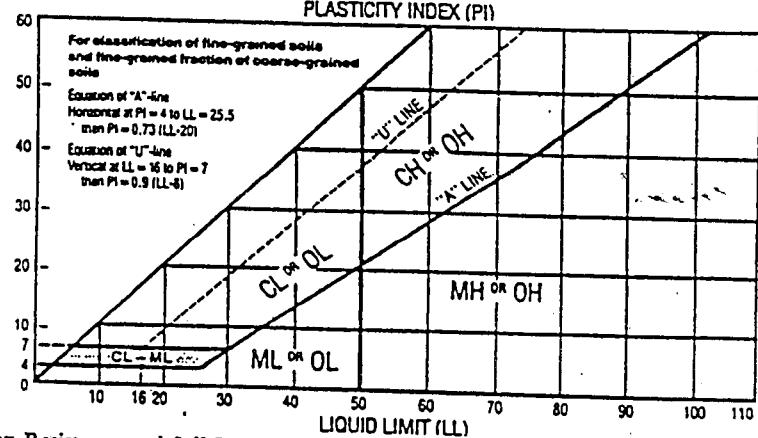
If soil contains $\geq 30\%$ plus No. 200, predominantly gravel, add "gravelly" to group name.

PI > 4 and plots on or above "A" line.

PI < 4 or plots below "A" line.

PI plots on or above "A" line.

PI plots below "A" line.



**Penetration Resistance and Soil Properties
on Basis of the Standard Penetration Test**

| Sands (Fairly Reliable) | | Clays (Rather Unreliable) | |
|----------------------------|------------------|------------------------------|-------------|
| No. of Blows per ft, N | Relative Density | No. of Blows per ft, N | Consistency |
| 0 - 4 | Very loose | Below 2 | Very soft |
| 4-10 | Loose | 2 - 4 | Soft |
| 10-30 | Medium | 4 - 8 | Medium |
| 30-50 | Dense | 8-15 | Stiff |
| Over 50 | Very dense | 15-30 | Very stiff |
| | | Over 30 | Hard |

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GRADATION CURVES

Lab. No: 16408

Sampled By: CK

Date Sampled: 1/6/2010

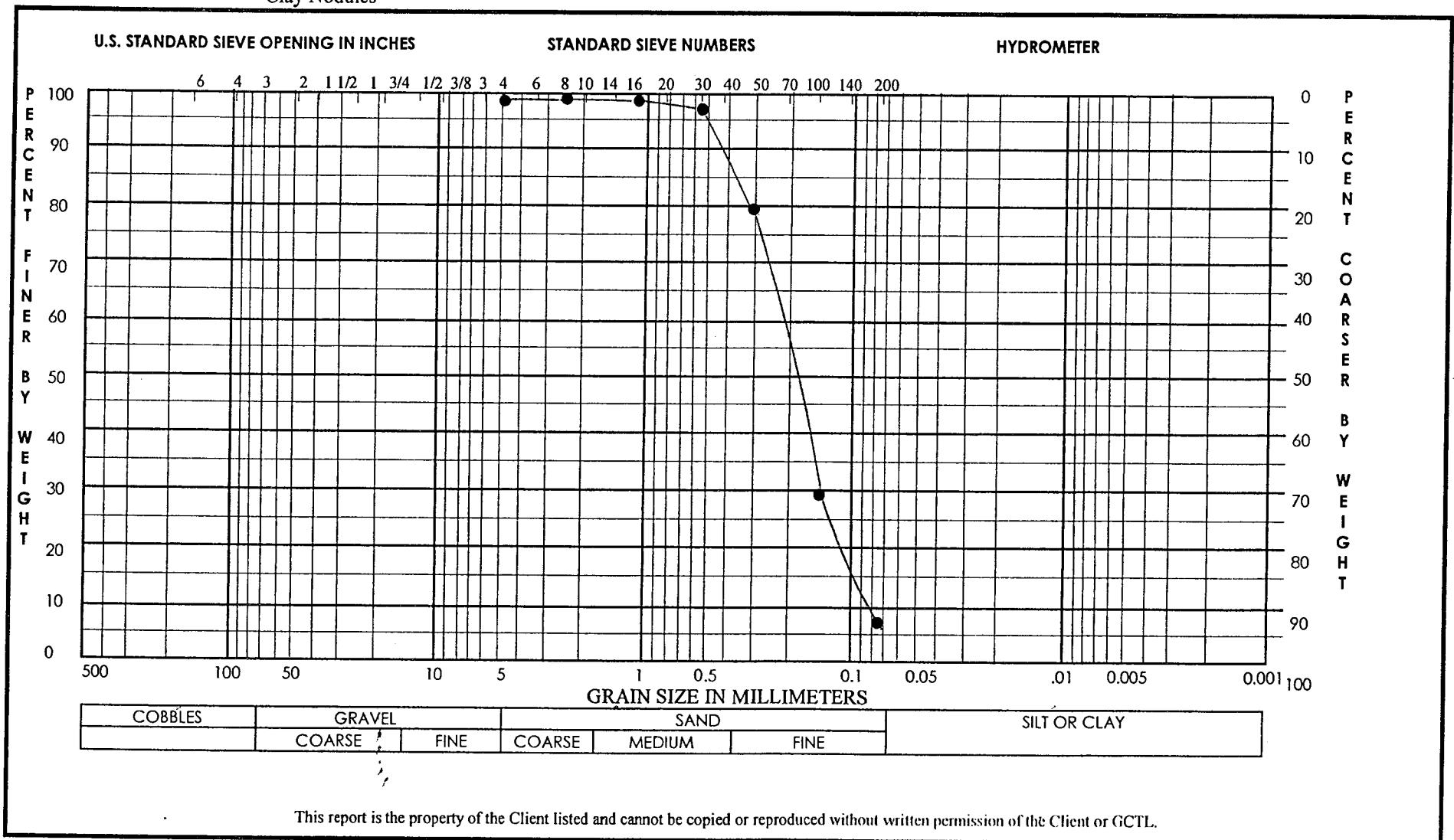
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Reddish Brown Sand with Few Rock Fragments and Occasional Clay Nodules

Source of Supply: On Site

Sampled From: Boring # 1, Sample # 2



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GRADATION CURVES

Lab. No: 16408

Sampled By: CK

Date Sampled: 1/6/2010

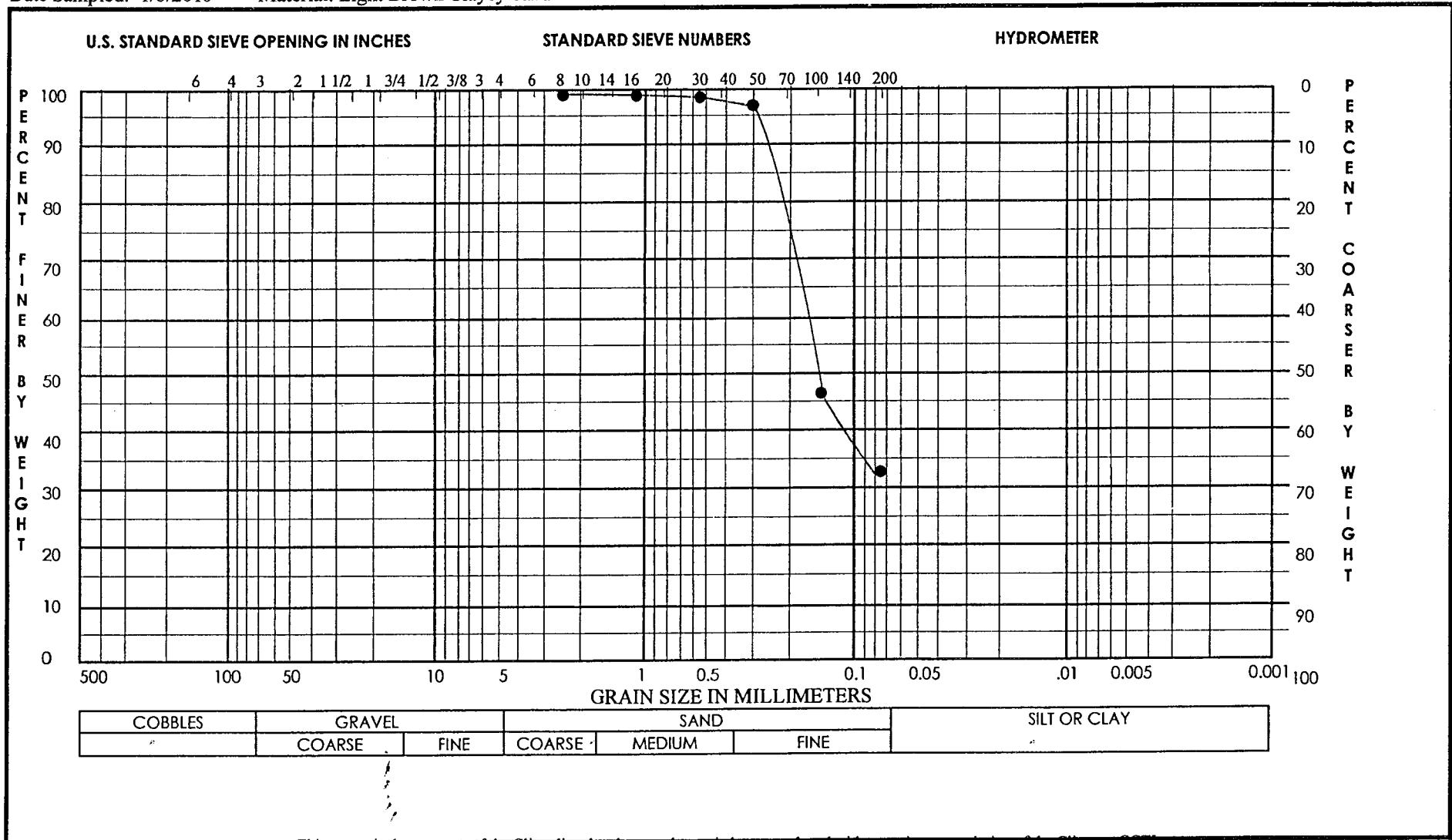
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Light Brown Clayey Sand

Source of Supply: On Site

Sampled From: Boring # 1, Sample # 9



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GRADATION CURVES

Lab. No: 16408

Project: 19305 Gulf Boulevard, Indian Shores

Source of Supply: On Site

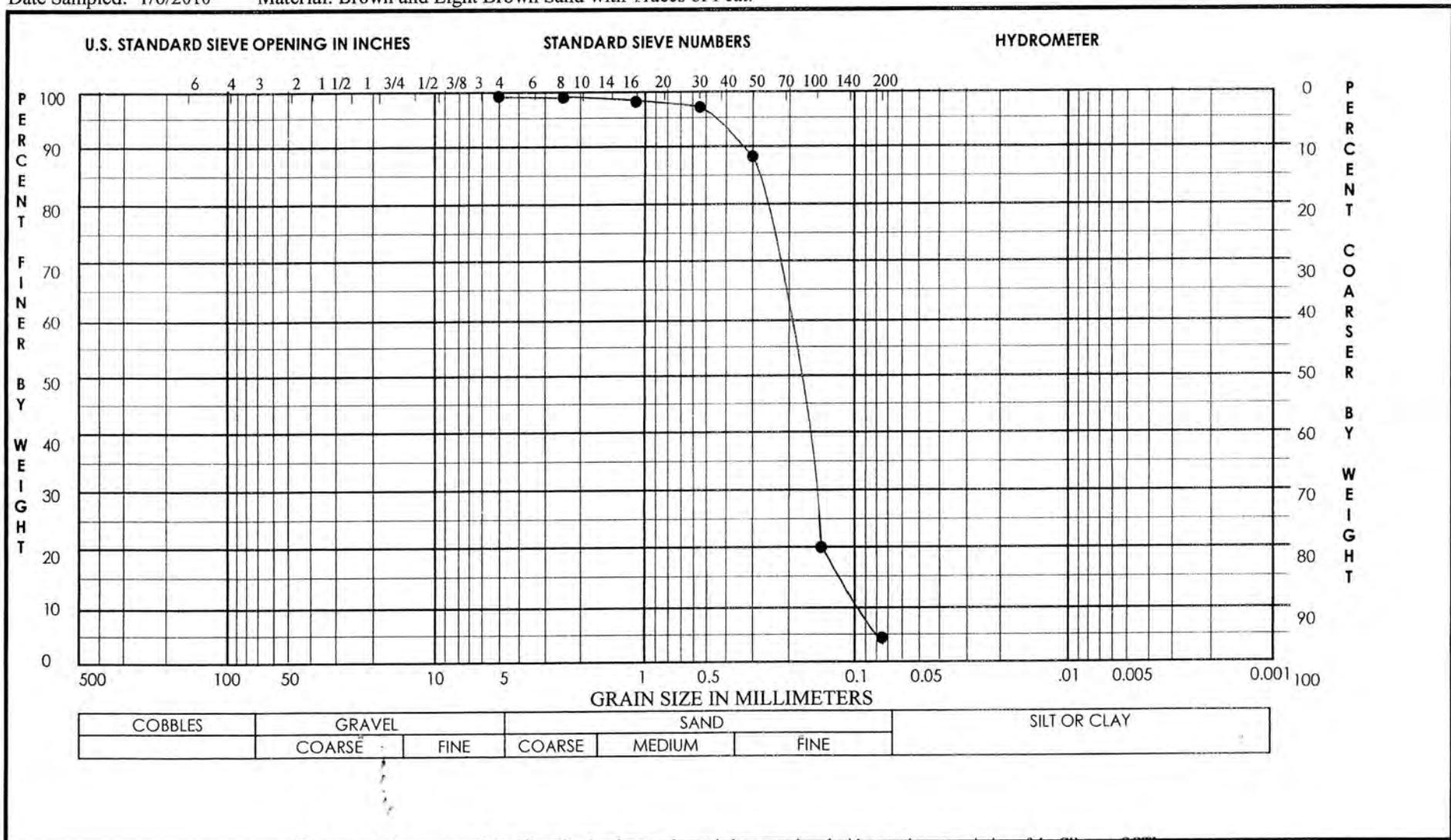
Sampled By: CK

Client: City of Indian Shores

Sampled From: Boring # 2, Sample # 4

Date Sampled: 1/6/2010

Material: Brown and Light Brown Sand with Traces of Peat.



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GRADATION CURVES

Lab. No: 16408

Sampled By: CK

Date Sampled: 1/6/2010

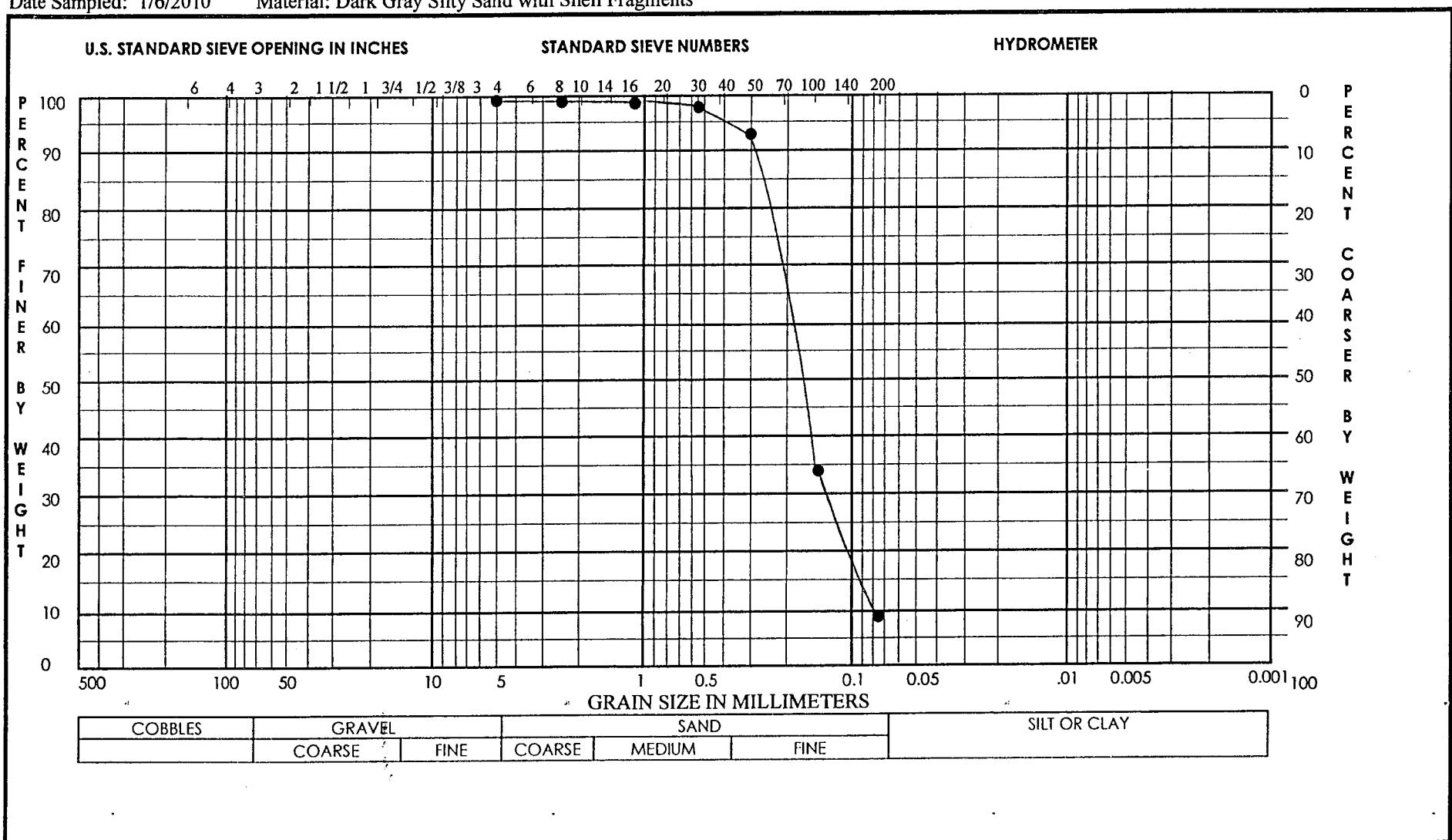
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Dark Gray Silty Sand with Shell Fragments

Source of Supply: On Site

Sampled From: Boring # 2, Sample # 7



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GRADATION CURVES

Lab. No.: 16408

Sampled By: CK

Date Sampled: 1/6/2010

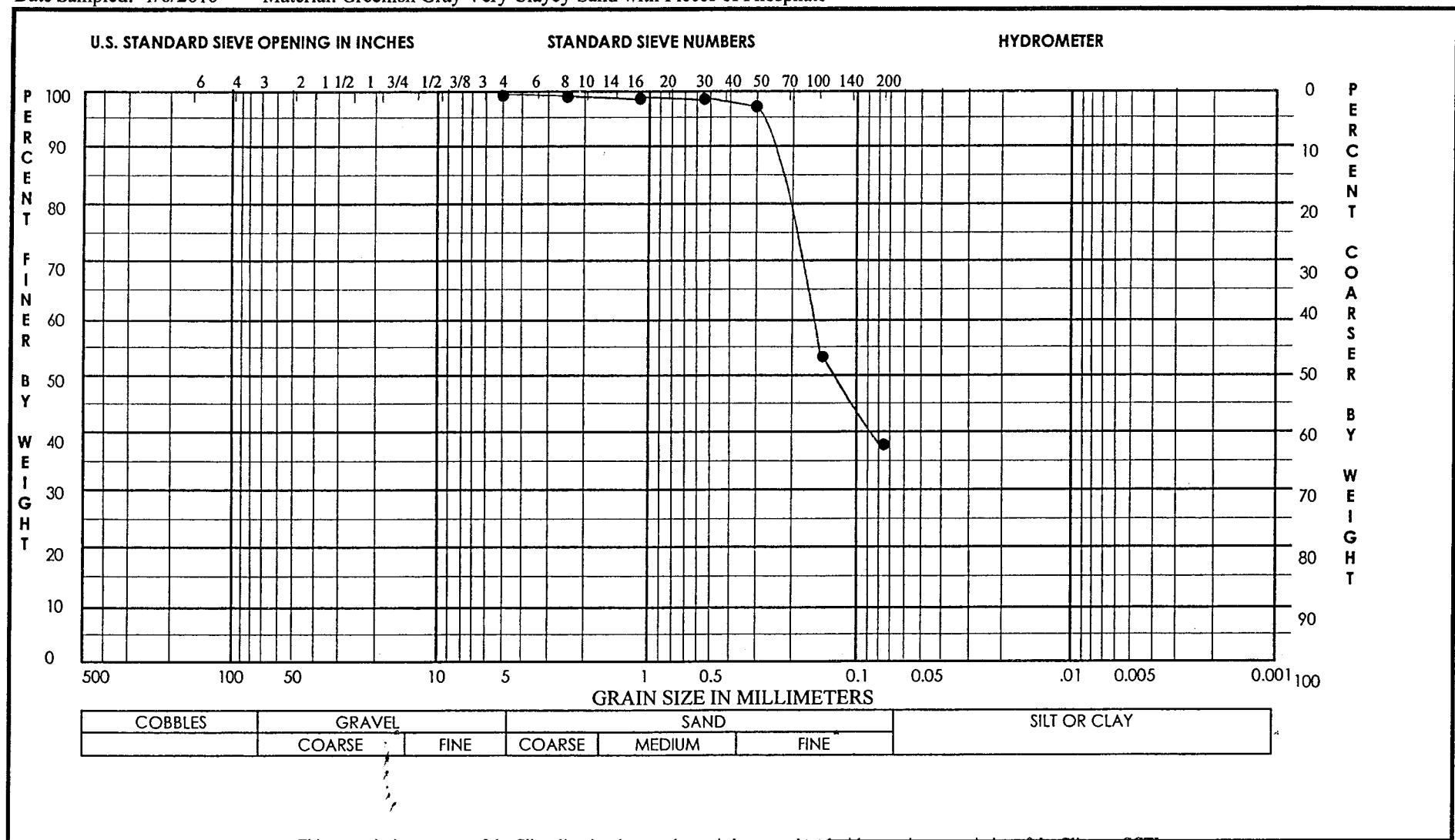
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Greenish Gray Very Clayey Sand with Pieces of Phosphate

Source of Supply: On Site

Sampled From: Boring # 2, Sample # 8



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GRADATION CURVES

Lab. No.: 16408

Sampled By: CK

Date Sampled: 1/6/2010

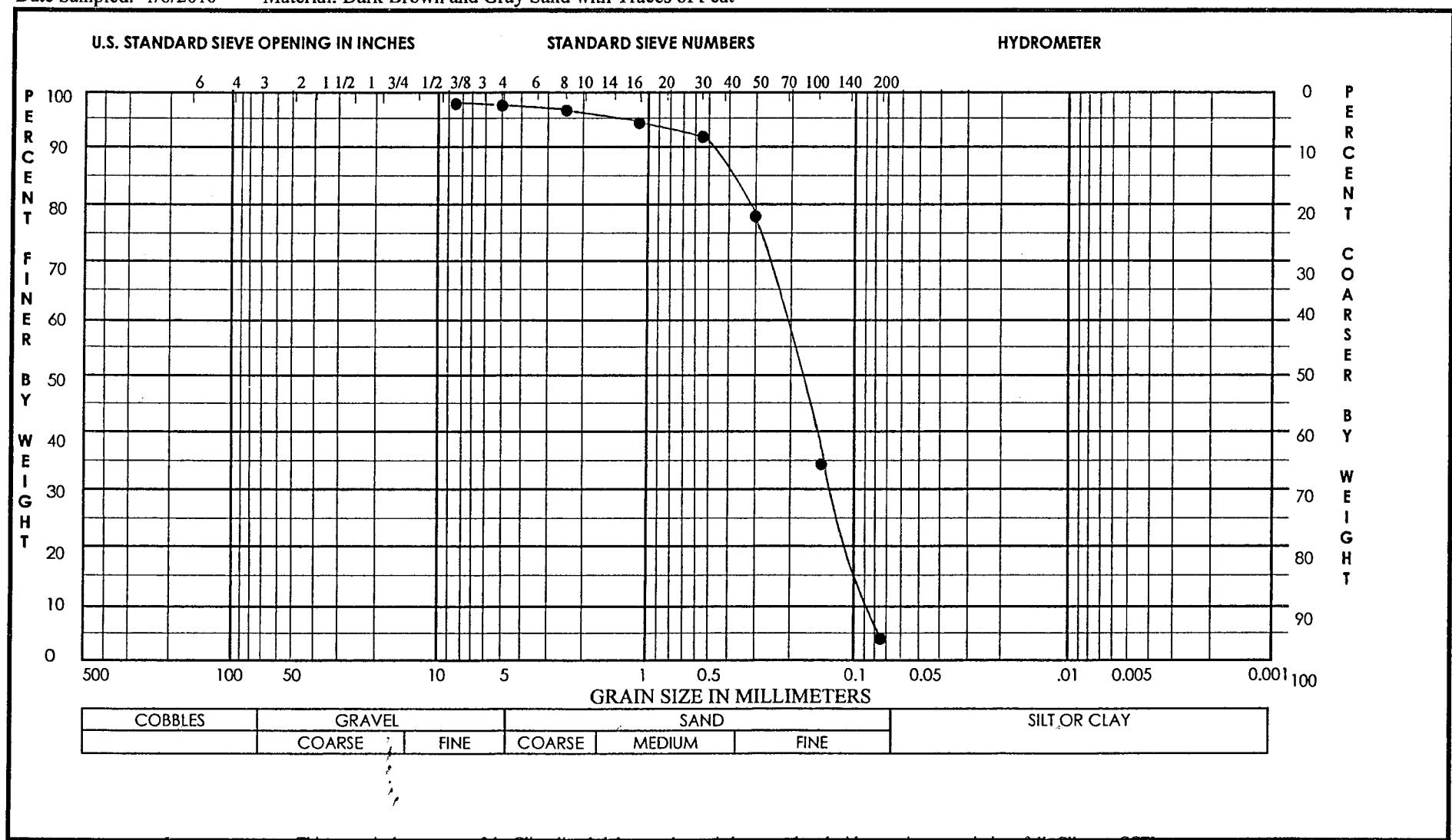
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Dark Brown and Gray Sand with Traces of Peat

Source of Supply: On Site

Sampled From: Boring #3, Sample #3



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GRADATION CURVES

Lab. No: 16408

Sampled By: CK

Date Sampled: 1/6/2010

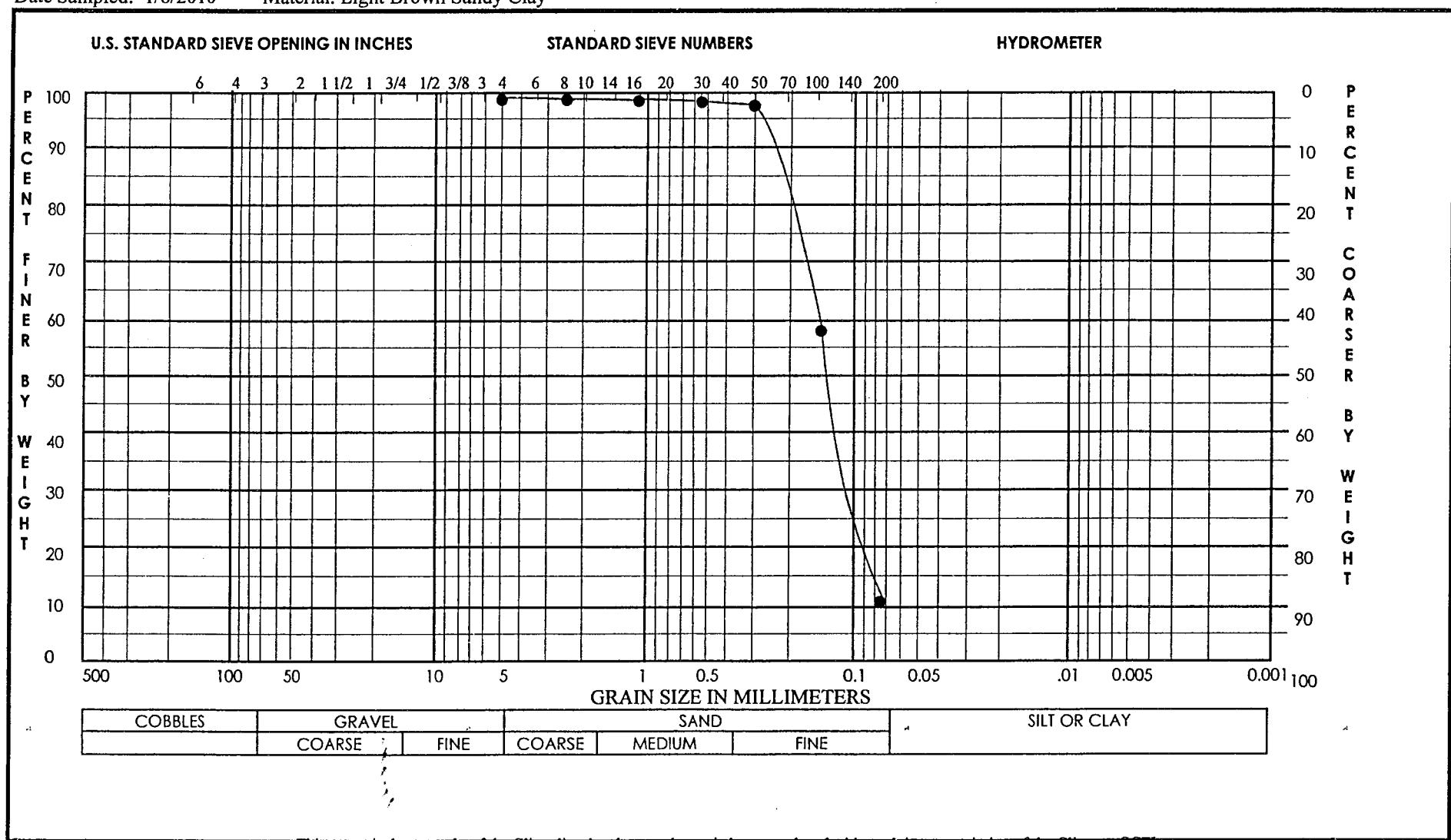
Project: 19305 Gulf Boulevard, Indian Shores

Client: Town of Indian Shores

Material: Light Brown Sandy Clay

Source of Supply: On Site

Sampled From: Boring #3, Sample #10



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Pinellas Park, FL 33781

Phone: (727) 544-4080

Moisture, Ash and Organic Matter of Peat and Organic Soils

FDOT/AASHTO T-267 ASTM D-2974

| | | | | | |
|------------------------|---|-------|----------|--------------|-----------------------------|
| Lab No.: | 16408 | Date: | 1/6/2010 | Apparatus: | Muffle furnace 445+/-10C |
| Field Tech: | | RD | | Lab Tech: | |
| Project Name: | 19305 Gulf Blvd. | | | | |
| Project Location: | 19305 Gulf Blvd. | | | Contractor | |
| Client: | Town of Indian Shores | | | | |
| Sample Location 1. | Boring #2 | | | Depth Taken: | S-4 |
| Sample Location 2. | | | | Depth Taken: | |
| Sample Description 1.: | Light Brown and Brown Sand with Traces of Peat. | | | | |
| Sample Description 2.: | Dark Brown and Gray Sand with Traces of Peat. | | | | |

NOTE: All weights given below are measured in grams unless otherwise indicated.

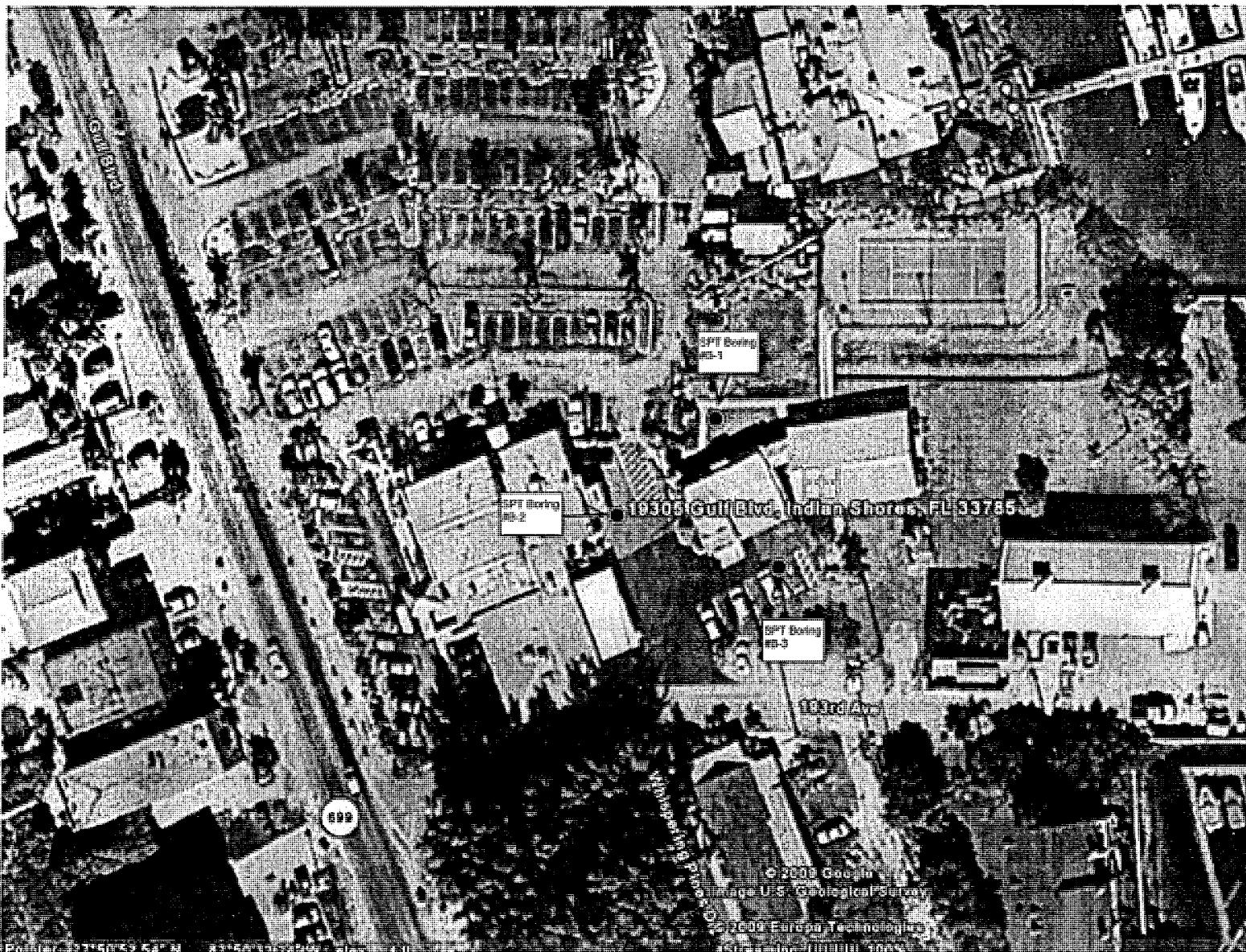
ASTM D-2974

Moisture, Ash, and Organic Matter of Peat and Organic Soils

| M%=[(Wet - Dry) x 100 / Dry] | | | Ash Content %=(ash x 100)/Dry) | | | Org. Matter% = 100.00 - Ash % | | |
|------------------------------|----------|----------|--------------------------------|----------|----------|-------------------------------|----------|----------|
| | Sample 1 | Sample 2 | | Sample 1 | Sample 2 | | Sample 1 | Sample 2 |
| Time In: | | | Time In: | 8:15am | | Time In: | | |
| Time Out: | | | Time Out: | | | Time Out: | | |
| | | | Tare | 47.26 | 56.03 | Tare | 47.26 | 56.03 |
| Wet | 105.40 | 119.80 | Dry | 124.20 | 151.00 | 100.00 | | |
| Dry | 77.00 | 95.10 | After burn | 122.46 | 149.05 | Ash % | 97.74 | 97.95 |
| Difference | 28.40 | 24.70 | Ash (w/o tare) | 75.20 | 93.02 | Organic % | 2.26 | 2.05 |
| Moisture% | 36.88 | 25.97 | Ash % | 97.74 | 97.95 | | | |

| FDOT/AASHTO T 267 Determination of Organic Content in Soils by Loss on Ignition | | | AASHTO T 11/ASTM C 117/ASTM D 422 Materials Finer than No. 200 Sieve by Washing / Particle-Size Analysis of Soils | | |
|--|-----------|----------|--|-----------------------------------|---------|
| Organic % =(A-B) / (A-C) x 100 | | | | | |
| | | Sample 1 | Sample 2 | Method followed using # 230 sieve | |
| Time In: | | | | Original | |
| Time Out: | | | | After Wash | |
| A=Before ignition w/ crucible | | 124.2 | 151.00 | Difference | |
| B=after ignition w/ crucible | | 122.46 | 149.05 | | |
| C=Crucible | | 47.26 | 56.03 | | |
| | Organic % | 2.26 | 2.05 | % Passing #230 | #DIV/0! |
| | | | | | #DIV/0! |

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Gulf Coast Testing Laboratory Inc
Lab #16408 Date: 1/6/10

19305 Gulf Blvd.
Indian Shores, FL

Proposed Four Story Building

Aerial View of Site and Boring Locations

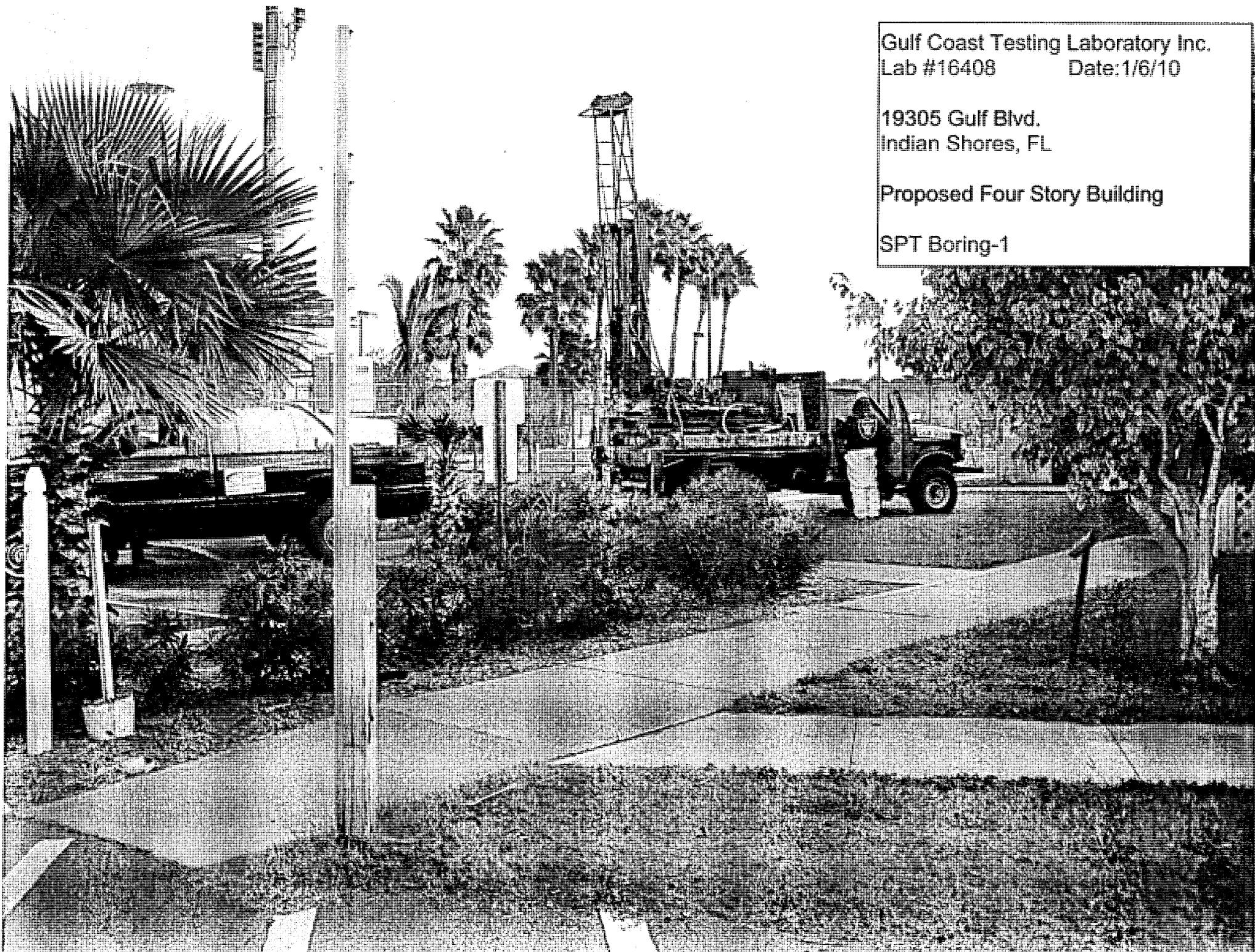
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Proposed Four Story Building

SPT Boring-1

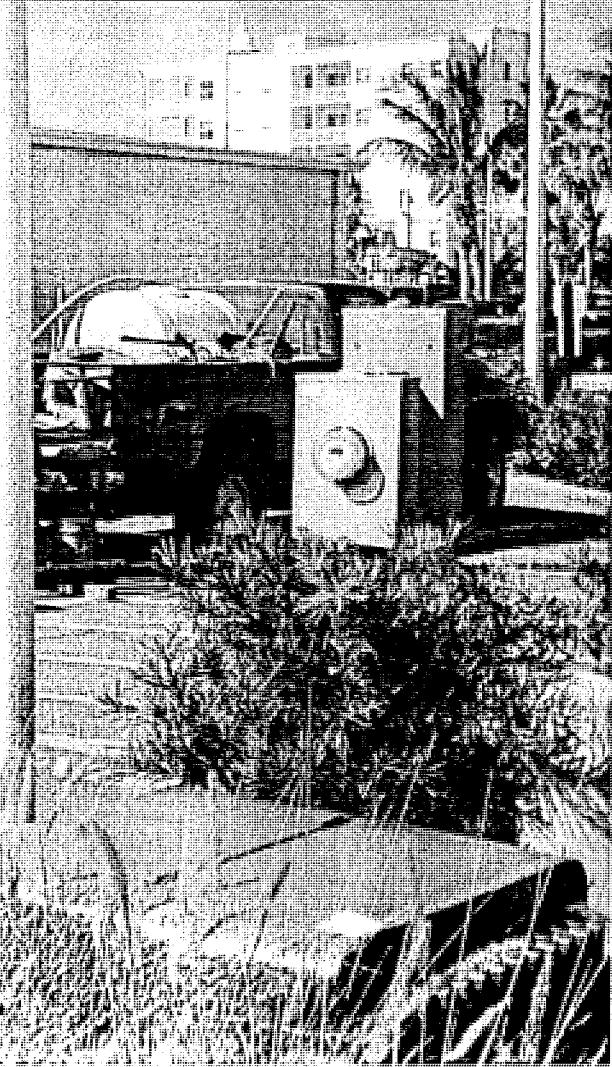


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SPT Boring-2

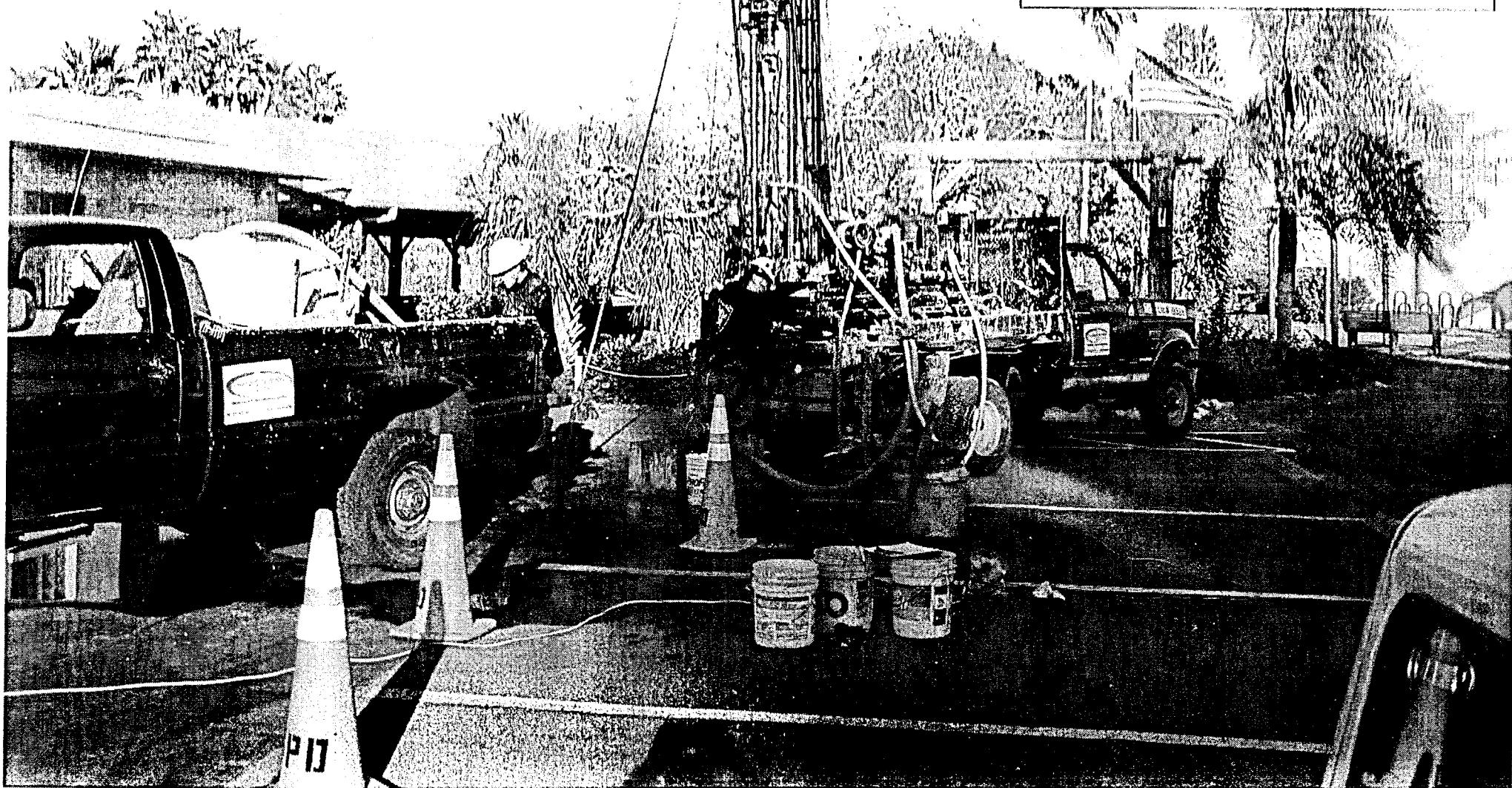


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Indian Shores, FL

Proposed Four Story Building

SPT Boring-3



Sharon Cornetet

From: Tyler Lohmiller <tlohmler@certusbuilders.com>
Sent: Thursday, November 14, 2013 11:33 AM
To: Sharon Cornetet; merrill@arc-3.com
Subject: Indian Shores Pavilion - Site Specific Soil Report

Chief/Merill,

The structural plans call for the G.C./Owner to obtain a site specific soil report. Has one already been completed, the Geotechnical Report from the new Municipal Building would work to satisfy the requirement. If so, can you forward that geotechnical report to me for my records.

Thank you,

Tyler J. Lohmiller, LEED AP

Project Manager



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304 S. Westland Ave
Tampa, FL 33606
904.210.2640
813.463.0266 fax
www.certusbuilders.com

emailed 11/15/13 10:34 a.m.

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11-25-13